# Quick Switching System with Different Reference Plans 

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#### Abstract

A new sampling inspection system with normal single sampling plan and tightened double sampling plan is introduced. Advantages of this system are highlighted.


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## 1. Introduction

Sampling system is a procedure used to accept or reject the lots in the acceptance sampling [1]. Dodge [2] proposed a new sampling inspection system called "Quick Switching System (QSS-1)". It is operated as follows:

1. Adopt a normal plan (N) and a tightened plan (T), where plan T has a tighter OC Curve than plan N .
2. Use plan N for the first lot. It is also possible to start with plan T when addition protection in the first lot production is desired. The OC curve properties are the same for the both plans.
3. For each is lot inspected; if the lot is accepted, then use plan N for the next lot; and if the lot is rejected, then use plan T for the next lot.

Rombaski [3] studied the QSS-1 with single sampling plan as a reference plan. After comparing the switching rules of many systems, Rombaski [3] made certain modifications on the switching rules of QSS-1. The resulting systems are QSS-2 and QSS-3. These systems are having an operating characteristic curve (OC) which is more discriminating than the corresponding OC curves of normal and tightened plans. Also the sample size required for QSS is much lower than any comparable equivalent sampling plan and system.

## 2. Literature Review

Soundarajan and Arumainayagam [4-11] have analyzed QSS-r, $\mathrm{r}=1,2,3$ with single sampling plan, double sampling plan, chain sampling plan and repetitive group sampling plan as reference plan. Arumainayagam and Uma $[12,13,14,15]$ studied QSS-r, $r=1,2,3$ with three stage multiple sampling plan as a reference plan. Suresh and Jeyalakshmi $[16,17,18]$ used multiple deferred sampling plans (MDS) as reference plan in QSS-1. Suresh and Kaviyarasu $[19,20]$ have analyzed QSS-r with conditional repetitive group (CRGS) sampling plan, two
stage CRGS plan and multiple repetitive groups sampling plan as a reference plans.

Arumainaygam and Vennila [21] have applied two different types of reference plans in QSS-1 and find that the resulting system is more advantages than the system using same reference plan for normal and tightened inspection. This paper extends this method to a system involving the switching roles of QSS-3.

## 3. Methodology

### 3.1. Quick Switching Single Double Sampling System (QSSDSS-3)

The new system incorporate the switching rules of QSS-3 with single sampling plan as normal plan and double sampling plan as the tightened plan. This system is called quick switching single double sampling system designated as QSSDSS - $3\left(\mathrm{n} ; \mathrm{c} ; \mathrm{c}_{1}, \mathrm{c}_{2}\right)$. Here n and c are the parameters of the normal plan and $\mathrm{n}\left(\mathrm{n}=\mathrm{n}_{1}=\mathrm{n}_{2}\right), \mathrm{c}_{1}$ and $\mathrm{c}_{2}$ are the parameters of the tightened plan. The sample sizes of the normal plan and tightened plan are equal where as $c_{1}<c_{2}<c$.

### 3.2. Conditions for applications

a) The production is stable so that outcome on current and preceding lots are broadly investigative of a continuing process and proposed lots are expected to be effectively of the same quality.
b) Lots are submitted substantially in order of their production.
c) Inspection by attributes is considered with quality defined as fraction nonconforming $p$.

### 3.3. Operating Procedure of QSSDSS-3 ( $\mathbf{n} ; \mathbf{c} ; \mathbf{c}_{1}, \mathbf{c}_{2}$ )

Step 1: From a lot, take a random sample of size n at normal inspection level and count the number of defectives x .
i) If $\mathrm{x} \leq \mathrm{c}$, accept the lot and repeat step 1 for the next lot.
ii) If $\mathrm{x}>\mathrm{c}$, reject the lot and go to step 2 .

Step 2: From the next lot, take a random sample of size n at tightened inspection level and count the number of defectives $\mathrm{x}_{1}$
i) If $\mathrm{x}_{1} \leq \mathrm{c}_{1}$, then accept the lot and repeat step 1 for the next lot
ii) If $\mathrm{x}_{1}>c_{2}$, then reject the lot and continue step 2 for the next lot.
iii) If $\mathrm{c}_{1}<\mathrm{x}_{1} \leq \mathrm{c}_{2}$, then take a second random sample of size n form the same lot, and count the number of defectives $x_{2}$.
iv) If $\mathrm{x}_{1}+\mathrm{x}_{2} \leq \mathrm{c}_{2}$, then accept the lot and repeat step 1 for the next lot
v) If $x_{1}+x_{2}>c_{2}$, then reject the lot and repeat step 2 for the next lot.

### 3.4. Operating Characteristic Function

Based on Romboski [3], the OC function of QSSDSS -3 ( $\mathrm{n} ; \mathrm{c} ; \mathrm{c}_{1}, \mathrm{c}_{2}$ ) is given below

$$
\begin{equation*}
P a(p)=\frac{P_{N} P_{T}^{3}+P_{T}\left(1-P_{N}\right)\left(P_{T}^{2}+P_{T}+1\right)}{P_{T}^{3}+\left(1-P_{N}\right)\left(P_{T}^{2}+P_{T}+1\right)} \tag{1}
\end{equation*}
$$

## Where

$\mathrm{P}_{\mathrm{N}}=$ Probability of acceptance of normal single sampling plan
$\mathrm{P}_{\mathrm{T}}=$ Probability of acceptance of tightened double sampling plan

## 4. Findings and Discussion

### 4.1. Properties of OC Curve

The properties of OC curve of QSSDSS-3 are given below

1. Figure 1 - Figure 3 give the normal, tightened and composite OC curve of QSSDSS - 3. The composite OC curve lies between normal and tightened OC curves. For good quality, the normal plan has more probability being applied in the system and hence it is closer to the composite OC curve. From these curves; it is observed that the relationship of the switching systems of composite OC curve is a weighted average of the normal and tightened OC curves. Incorporating the advantages of normal and tightened OC curve the composite OC curve attains more desirable form than the two OC curves.


Figure 1. Normal, Tightened and Composite OC curves of QSSDSS - $3\left(n ; c ; c_{1}, c_{2}\right), \operatorname{QSSDSS}-3(100,2,0,1)$


Figure 2. Normal, Tightened and Composite OC curves of QSSDSS - $3\left(\mathrm{n} ; \mathrm{c} ; \mathrm{c}_{1}, \mathrm{c}_{2}\right)$, $\operatorname{QSSDSS}-3(150,5,0,3)$


Figure 3. Normal, Tightened and Composite OC curves of QSSDSS - 3 ( $n ; c ; c_{1}, c_{2}$ ), $\operatorname{QSSDSS}-3(175,4,1,3)$


Figure 4. Composite OC curves of (QSSDSS-3) ( $\mathrm{n} ; \mathrm{c} ; \mathrm{c}_{1}, \mathrm{c}_{2}$ ); 1.QSSDSS-3 (225, 5, 0, 4); 2.QSSDSS-3 (225, 5, 0, 3); 3.QSSDSS-3 (225, 5, 0,2 ); 4. QSSDSS-3 (225, 5, 0, 1)
2. Figure 4 give a set of composite OC curves of the QSSDSS. In these curves, the normal plan is fixed and in the tightened plan acceptance number is allowed to decrease. That is tightening is made severe. It is observed that as the value of p increases, the OC curve approaches to the shape of an ideal OC curve.

### 4.2. Designing the System

### 4.2.1. Designing Systems Given $p_{1}, p_{2}, \alpha$ and $\beta$

Table 3 can be used to design QSSDSS - 3 ( $\mathrm{n}, \mathrm{c}, \mathrm{c}_{1}, \mathrm{c}_{2}$ ) for given $p_{1}, p_{2}, \alpha$ and $\beta$ by the following steps:

1. Find the value of $p_{2} / p_{1}$.
2. Determine the value of $p_{2} / p_{1}$ in Table 4 in the column for appropriate $\alpha$ and $\beta$ that is closer to the computed $p_{2} / p_{1}$.

3 . Find the values of $c, c_{1}$ and $c_{2}$ corresponding to the ratio located.
4. Corresponding to the selected $\mathrm{c}, \mathrm{c}_{1}$ and $\mathrm{c}_{2}$, from Table 3, find the value of $\mathrm{np}_{1}$
5. The sample size of the system is found by dividing $\mathrm{np}_{1}$ by $\mathrm{p}_{1}$.

Example:
To obtain QSSDSS - $3\left(\mathrm{n}, \mathrm{c}, \mathrm{c}_{1}, \mathrm{c}_{2}\right.$ ) for the given values
of $\mathrm{p}_{1}=0.03, \alpha=0.05, \mathrm{p}_{2}=0.04$ and $\beta=0.10$, the following steps are to be followed:

1. Compute $\mathrm{p}_{2} / \mathrm{p}_{1}=0.04 / 0.03=1.33$
2. The value of $\mathrm{p}_{2} / \mathrm{p}_{1}$ which is nearly equal to 1.3 in Table 4 under the column of $\alpha=0.05$ and $\beta=0.10$ is 1.3429

3 . The value of $c, c_{1}$ and $c_{2}$ corresponding to 1.3429 are $\mathrm{c}=10, \mathrm{c}_{1}=0, \mathrm{c}_{2}=2$.
4. For $\mathrm{c}=10, \mathrm{c}_{1}=0, \mathrm{c}_{2}=2$, value of $\mathrm{np}_{1}$ obtained from Table 3 is 2.8306 .
5. The sample size is determined as $n=\mathrm{np}_{1} / \mathrm{p}_{1}=$ $2.8306 / 0.03=94$.
6. The designed system is QSSDSS - 3 (94; 10, 0, 2).

### 4.2.2. Calculating AOQL for the given system

Table 5 provides the $\mathrm{np}_{\mathrm{m}}$ and nAOQL values for QSSDSS - 3 ( $\mathrm{n}, \mathrm{c}, \mathrm{c}_{1}, \mathrm{c}_{2}$ ). This table can be used to determine $\mathrm{np}_{\mathrm{m}}$ and nAOQL of a system.

Example:
Determine the $\mathrm{p}_{\mathrm{m}}$ and AOQL of QSSDSS - 3 (94, 4, 0, 2). From Table 5, corresponding to $\mathrm{c}=10, \mathrm{c}_{1}=0$ and $\mathrm{c}_{2}=2$, $\mathrm{nAOQL}=4.3333$ and $\mathrm{np}_{\mathrm{m}}=4.7960$. so $\mathrm{AOQL}=\mathrm{nAOQL}$ $/ \mathrm{n}=4.3333 / 94=0.046 \%$ and $\mathrm{p}_{\mathrm{m}}=\mathrm{np}_{\mathrm{m}} / \mathrm{n}=4.7960 / 94$ $=0.05 \%$.

### 4.2.3. Designing Systems Given AQL and AOQL

Table 5 can be used to design QSSDSS - 3 ( $\mathrm{n}, \mathrm{c}, \mathrm{c}_{1}, \mathrm{c}_{2}$ ) for specified values of AQL and AOQL.

Example
To determine a QSSDSS - $3\left(\mathrm{n} ; \mathrm{c} ; \mathrm{c}_{1}, \mathrm{c}_{2}\right.$ ), having AQL $(\alpha=0.05)=0.06$ and $\mathrm{AOQL}=0.08$, compute $\mathrm{AOQL} / \mathrm{p}_{1}=$ $0.08 / 0.06=1.3$. From Table 5, under the column headed $\mathrm{AOQL} / \mathrm{p}_{1}$, value closer to the desired value is 1.3119 , which corresponds to a value of $\mathrm{c}=9, \mathrm{c}_{1}=0$ and $\mathrm{c}_{2}=3$. Corresponding to these parameters, value of $\mathrm{np}_{1}$ obtained from Table 5 is 3.0601 . The normal single sampling plan sample size is obtained by $\mathrm{n}=\mathrm{np}_{1} / \mathrm{p}_{1}=3.0601 / 0.06=$ 51. The designed system is QSSDSS - 3 (51; $9 ; 0,3$ ).

### 4.2.4. Designing Systems Given Indifference Quality Level (IQL)

Table 5 can be used to design QSSDSS - $3\left(\mathrm{n} ; \mathrm{c} ; \mathrm{c}_{1}, \mathrm{c}_{2}\right.$ ) indexed by point of control and point of control $\left(h_{0}\right)$ Hamaker [22]

Example
If one wants to design a QSSDSS-3 having $\mathrm{p}_{0}=0.03$ and $h_{0}=2.6$, from Table 3, under the column headed $h_{0}$ find the value which is closer to the desired value. The value is 2.5782 which has associated with it a value of $\mathrm{c}=$ $3, c_{1}=0$ and $c_{2}=2$. Corresponding to these parameters, value of $\mathrm{np}_{0}$ is 1.9059 . The sample size of normal double sampling plan is obtained as $n=\mathrm{np}_{0} / \mathrm{n}=1.9059 / 0.03=$ $63.53 \approx 64$. The designed system is QSSDSS - $3(64 ; 3 ; 0,2)$.

### 4.2.5. Conversion of One Set of Parameters to Other

For QSSDSS - $3\left(\mathrm{n} ; \mathrm{c} ; \mathrm{c}_{1}, \mathrm{c}_{2}\right.$ ), if $\mathrm{p}_{1}=0.02, \mathrm{p}_{2}=0.04$, $\alpha=0.05$ and $\beta=0.10$, the system satisfying the requirements can be obtained from Table 5 as $\mathrm{n}=94, \mathrm{c}=10, \mathrm{c}_{1}=0$ and $\mathrm{c}_{2}=2$. Corresponding to $\mathrm{c}=10, \mathrm{c}_{1}=0$ and $\mathrm{c}_{2}=2$, from Tables 3 , one can get the following:
$\mathrm{np}_{1}=2.8306, \mathrm{np}_{\mathrm{m}}=4.7960, \mathrm{nAOQL}=4.3330$
$\mathrm{np}_{0}=3.3278$ and $\mathrm{h}_{0}=4.8118$.
$\mathrm{So}, \mathrm{AOQL}=\mathrm{nAOQL} / \mathrm{n}=4.3330 / 94=0.0461$
$\mathrm{p}_{0}=\mathrm{np}_{0} / \mathrm{n}=3.3278 / 94=0.0354$.
So, when $p_{1}=0.02, \alpha=0.05, p_{2}=0.04$ and $\beta=0.10$, the other similar sets of parameters are given by

1. $\mathrm{p}_{1}=0.02(\alpha=0.05)$ and $\mathrm{AOQL}=0.0461$
2. $\mathrm{p}_{0}=0.0354$ and $\mathrm{h}_{0}=4.8118$.

### 4.3. Plotting the OC Curve

Table 1 can be used to plot the operating characteristic curve of the given QSSDSS - $3\left(\mathrm{n} ; \mathrm{c} ; \mathrm{c}_{1}, \mathrm{c}_{2}\right.$ ). This can be done by dividing each entry for given acceptance numbers, by the value of $n$. The result of each division is the proportion nonconforming $p$ for which the proportion of lots expected to be accepted $\mathrm{P}_{\mathrm{a}}(\mathrm{p})$ is shown in the corresponding column heading.

Example
For QSSDSS - 3 (60; 3; 0, 1), division of entries opposite to $\mathrm{c}=3, \mathrm{c}_{1}=0$ and $\mathrm{c}_{2}=1$ in Table 3 by 100 leads to the following Table-A for plotting the OC curve of QSSDSS-3.

Table 1. Values for OC curve of (QSSDSS - 3) ( $\left.n ; c ; c_{1} ; c_{2}\right)\left(n=n_{1}=n_{2}\right)$ ( $60,3,0,1$ )

| $\mathrm{Pa}(\mathrm{p})$ | 0.99 | 0.95 | 0.75 | 0.50 | 0.25 | 0.10 | 0.05 | 0.01 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P | 0.0103 | 0.0141 | 0.0195 | 0.0239 | 0.0304 | 0.0418 | 0.0521 | 0.0775 |

## 5. Conclusion

### 5.1. Comparison

The last three columns of below Table 2 respectively give the values obtained by dividing the $n p_{0.95}$ values of $\operatorname{SSP}\left(\mathrm{n} ; \mathrm{c}_{\mathrm{N}}, \mathrm{c}_{\mathrm{T}}\right)$ (values are taken from Cameron J.M., [23]), DSP ( $\mathrm{n} ; \mathrm{c}_{\mathrm{N}}, \mathrm{c}_{\mathrm{T}}$ ) (Duncun A.J., [24]), (US Chemical Corps Agency [25]) and QSS-3 ( $n ; c_{\mathrm{N}}, \mathrm{c}_{\mathrm{T}}$ ) (Romboski L.D. [3] respectively) by the $n p_{0.95}$ value of the matched QSSDSS-3 ( $n ; c, c_{1} ; c_{2}$ ). Six single sampling plans, double sampling plan, and QSS - 3 their equivalent QSSDSS-3 ( $\mathrm{n}, \mathrm{c}, \mathrm{c} 1$, c2) values are presented in the below table. From this, one can observe the following, On comparing the $\mathrm{np}_{0.95}$ values of different systems included in various sets, it is observed that the sample size of QSSDSS-3 $\left(\mathrm{n} ; \mathrm{c}, \mathrm{c}_{1} ; \mathrm{c}_{2}\right.$ ) requires lesser sample sizes than those of the corresponding matched $\operatorname{SSP}\left(n ; c_{N}, c_{T}\right)$, DSP ( $n ; c_{N}, c_{T}$ ) and QSS-3 ( $\mathrm{n} ; \mathrm{c}_{\mathrm{N}}, \mathrm{c}_{\mathrm{T}}$ ). However, in some cases, QSSDSS-3 $\left(\mathrm{n} ; \mathrm{c}, \mathrm{c}_{1} ; \mathrm{c}_{2}\right.$ ) requires a smaller sample size than that of $\operatorname{QSS}-3\left(n ; c_{N}, c_{T}\right)$.

Table 2. Single, Double and QSSDSS - 3 Comparison Values

| SSP |  |  | DSP |  |  |  | QSS-3 |  |  |  | QSSDSS-3 |  |  |  |  | *E1 | * $\mathbf{E} 2$ | *E3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| c | OR | np0.95 | a1 | a2 | OR | np0.95 | cn | ct | OR | np0.95 | c | c1 | c2 | OR | np0.95 |  |  |  |
| 6 | 3.21 | 3.29 | 3 | 7 | 3.21 | 2.15 | 5 | 4 | 3.22 | 2.49 | 3 | 0 | 2 | 3.17 | 1.00 | 3.28 | 2.15 | 2.49 |
| 7 | 2.96 | 3.98 | 2 | 8 | 2.93 | 2.36 | 5 | 3 | 2.93 | 2.88 | 3 | 0 | 1 | 2.96 | 0.85 | 4.70 | 2.78 | 3.40 |
| 8 | 2.77 | 4.70 | 5 | 10 | 2.76 | 3.40 | 7 | 6 | 2.74 | 3.86 | 4 | 1 | 2 | 2.78 | 1.58 | 2.97 | 2.15 | 2.44 |
| 10 | 2.47 | 6.17 | 5 | 12 | 2.44 | 4.00 | 4 | 0 | 2.47 | 0.96 | 5 | 0 | 4 | 2.44 | 2.22 | 2.77 | 1.80 | 0.43 |
| 12 | 2.31 | 7.69 | 5 | 13 | 2.32 | 4.35 | 9 | 7 | 2.31 | 5.11 | 5 | 1 | 2 | 2.31 | 1.18 | 6.53 | 3.69 | 4.34 |
| 14 | 2.22 | 10.04 | 5 | 14 | 5.14 | 2.22 | 6 | 2 | 2.26 | 2.36 | 5 | 1 | 4 | 2.22 | 2.14 | 4.70 | 1.04 | 1.11 |

Where
*E1 $=\mathrm{np} 0.95$ of SSP $/ \mathrm{np} 0.95$ of QSSDSS-3
*E2 $=\mathrm{np} 0.95$ of DSP $/ \mathrm{np} 0.95$ of QSSDSS-3
*E3 $=$ np0.95 of QSS-3 / np0.95 of QSSDSS-3

Table 3. Values of $n p$ tabulated against $c, c_{1} \& c_{2}$ for give $\operatorname{Pa}(p)$ for $\operatorname{QSSDSS}-3\left(n, c, c_{1}, c_{2}\right)$

| $\mathbf{P a}(\mathbf{p})$ - Probability of Acceptance |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| c | $\mathrm{c}_{1}$ | $\mathbf{c}_{2}$ | 0.99 | 0.95 | 0.75 | 0.5 | 0.25 | 0.1 | 0.05 | 0.01 |
| 2 | 0 | 1 | 0.3747 | 0.5921 | 0.9406 | 1.2460 | 1.7327 | 2.4980 | 3.1257 | 4.6487 |
| 3 | 0 | 1 | 0.6202 | 0.8475 | 1.1718 | 1.4311 | 1.8242 | 2.5110 | 3.1277 | 4.6488 |
|  | 0 | 2 | 0.7401 | 1.0663 | 1.5351 | 1.9059 | 2.4396 | 3.1994 | 3.7820 | 5.1167 |
| 4 | 0 | 2 | 1.0447 | 1.3598 | 1.7775 | 2.0891 | 2.5266 | 3.2122 | 3.7841 | 5.1167 |
|  | 0 | 3 | 1.1811 | 1.6190 | 2.2211 | 2.6789 | 3.3113 | 4.1616 | 4.7839 | 6.1260 |
|  | 1 | 2 | 1.0685 | 1.4173 | 1.9119 | 2.3130 | 2.9330 | 3.9438 | 4.7664 | 6.6427 |
|  | 1 | 3 | 1.1643 | 1.5832 | 2.1644 | 2.6192 | 3.2802 | 4.2411 | 4.9911 | 6.7348 |
| 5 | 0 | 1 | 1.0984 | 1.3284 | 1.6269 | 1.8404 | 2.1202 | 2.5975 | 3.1424 | 4.6489 |
|  | 0 | 2 | 1.3301 | 1.6311 | 2.0135 | 2.2857 | 2.6487 | 3.2388 | 3.7885 | 5.1168 |
|  | 0 | 3 | 1.5361 | 1.9484 | 2.4793 | 2.8656 | 3.3939 | 4.1732 | 4.7858 | 6.1261 |
|  | 0 | 4 | 1.6776 | 2.2263 | 2.9646 | 3.5149 | 4.2574 | 5.2197 | 5.9054 | 7.3463 |
|  | 1 | 2 | 1.3760 | 1.7189 | 2.1813 | 2.5354 | 3.0549 | 3.9619 | 4.7690 | 4.7690 |
|  | 1 | 4 | 1.6387 | 2.1368 | 2.7944 | 3.2842 | 3.9620 | 4.9047 | 5.6140 | 7.1930 |
| 6 | 0 | 1 | 1.3307 | 1.5609 | 1.8527 | 2.0545 | 2.3047 | 2.6953 | 3.1663 | 4.6491 |
|  | 0 | 3 | 1.8643 | 2.2506 | 2.7303 | 3.0662 | 3.5088 | 4.1955 | 4.7895 | 6.1261 |
|  | 0 | 4 | 2.0749 | 2.5871 | 3.2371 | 3.7046 | 4.3357 | 5.2301 | 5.9071 | 7.3464 |
|  | 1 | 2 | 1.6718 | 2.0086 | 2.4478 | 2.7694 | 3.2131 | 3.9966 | 4.7741 | 6.6428 |
| 7 | 0 | 1 | 1.5600 | 1.7907 | 2.0781 | 2.2721 | 2.5024 | 2.8312 | 3.2171 | 4.6496 |
|  | 0 | 2 | 1.8551 | 2.1333 | 2.4715 | 2.6974 | 2.9696 | 3.3738 | 3.8196 | 5.1171 |
|  | 0 | 4 | 2.4414 | 2.9176 | 3.5022 | 3.9091 | 4.4442 | 5.2489 | 5.9102 | 7.3464 |
|  | 0 | 6 | 2.7883 | 3.5504 | 4.5521 | 5.2803 | 6.2316 | 7.4036 | 8.2128 | 9.8745 |
| 8 | 0 | 4 | 2.7811 | 3.2261 | 3.7608 | 4.1227 | 4.5810 | 5.2825 | 5.9160 | 7.3465 |
|  | 1 | 6 | 3.1466 | 3.7715 | 4.5406 | 5.0812 | 5.7994 | 6.8172 | 7.5895 | 9.2161 |
|  | 1 | 7 | 3.3113 | 4.0778 | 5.0522 | 5.7517 | 6.6762 | 7.8663 | 8.7043 | 10.4272 |
| 9 | 0 | 1 | 2.0137 | 2.2461 | 2.5293 | 2.7142 | 2.9215 | 3.1804 | 3.4366 | 4.6531 |
|  | 0 | 3 | 2.7304 | 3.0601 | 3.4494 | 3.7021 | 3.9957 | 4.4061 | 4.8434 | 6.1268 |
|  | 0 | 6 | 3.6809 | 4.3367 | 5.1306 | 5.6797 | 6.3992 | 7.4265 | 8.2165 | 9.8746 |
|  | 1 | 5 | 3.2713 | 3.7422 | 4.3031 | 4.6794 | 5.1508 | 5.8723 | 6.5418 | 8.0882 |
|  | 1 | 6 | 3.5411 | 4.1210 | 4.8183 | 5.2959 | 5.9155 | 6.8380 | 7.5929 | 9.2162 |
|  | 1 | 7 | 3.7633 | 4.4741 | 5.3452 | 5.9553 | 6.7612 | 7.8775 | 8.7061 | 10.4272 |
|  | 1 | 8 | 3.9285 | 4.7871 | 5.8739 | 6.6496 | 7.6650 | 8.9471 | 9.8387 | 11.6571 |
| 10 | 0 | 2 | 2.5734 | 2.8306 | 3.1344 | 3.3278 | 3.5408 | 3.8013 | 4.0509 | 5.1216 |
|  | 0 | 3 | 2.9926 | 3.3092 | 3.6801 | 3.9170 | 4.1843 | 4.5352 | 4.8994 | 6.1275 |
|  | 0 | 5 | 3.7657 | 4.2595 | 4.8407 | 5.2253 | 5.6981 | 6.4087 | 7.0759 | 8.6124 |
|  | 0 | 7 | 4.3311 | 5.0739 | 5.9686 | 6.5855 | 7.3913 | 8.5171 | 9.3636 | 11.1225 |
|  | 1 | 2 | 2.7837 | 3.1043 | 3.4954 | 3.7537 | 4.0528 | 4.4612 | 4.9201 | 6.6441 |
|  | 1 | 3 | 2.9645 | 3.2918 | 3.6843 | 3.9413 | 4.2389 | 4.6490 | 5.1067 | 6.7360 |
|  | 1 | 4 | 3.2629 | 3.6330 | 4.0700 | 4.3545 | 4.6876 | 5.1611 | 5.6739 | 7.1937 |
|  | 1 | 6 | 3.9081 | 4.4494 | 5.0901 | 5.5190 | 6.0577 | 6.8728 | 7.5989 | 9.2162 |
|  | 1 | 8 | 4.4037 | 5.2009 | 6.1743 | 6.8537 | 7.7466 | 8.9575 | 9.8403 | 11.6571 |

Table 4. Values of $p_{2} / \mathbf{p}_{1}$ tabulated against $\mathbf{c}, \mathrm{c}_{1} \& \mathbf{c}_{2}$ for given $\alpha$ and $\boldsymbol{\beta}$ for $\operatorname{QSSDSS}-3\left(\mathbf{n}, \mathrm{c}, \mathbf{c}_{1}, \mathbf{c}_{2}\right)$

| c | $\mathrm{c}_{1}$ | $\mathrm{c}_{2}$ | $\mathrm{p}_{2} / \mathrm{p}_{1}$ for |  |  | $\begin{aligned} & \mathrm{np}_{1} \text { for } \\ & \alpha=0.05 \end{aligned}$ | $\mathbf{p}_{2} / \mathbf{p}_{1}$ for |  |  | $\begin{gathered} \mathrm{np}_{1} \text { for } \\ \boldsymbol{\alpha}=\mathbf{0 . 0 1} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & \alpha=0.05 \\ & \beta=0.10 \end{aligned}$ | $\begin{aligned} & \alpha=0.05 \\ & \beta=0.05 \end{aligned}$ | $\begin{aligned} & \alpha=0.05 \\ & \beta=0.01 \end{aligned}$ |  | $\begin{aligned} \alpha & =0.01 \\ \beta & =0.10 \end{aligned}$ | $\begin{aligned} & \alpha=\mathbf{0 . 0 1} \\ & \boldsymbol{\beta}=\mathbf{0 . 0 5} \end{aligned}$ | $\begin{aligned} \alpha & =0.01 \\ \beta & =0.01 \end{aligned}$ |  |
| 2 | 0 | 1 | 4.2191 | 5.2791 | 7.8515 | 0.5921 | 6.6672 | 8.3423 | 12.4072 | 0.3747 |
| 3 | 0 | 1 | 2.9627 | 3.6903 | 5.4851 | 0.8475 | 4.0485 | 5.0429 | 7.4954 | 0.6202 |
|  | 0 | 2 | 3.0003 | 3.5467 | 4.7984 | 1.0663 | 4.3229 | 5.1102 | 6.9136 | 0.7401 |
| 4 | 0 | 2 | 2.3624 | 2.7829 | 3.7630 | 1.3598 | 3.0747 | 3.6220 | 4.8976 | 1.0447 |
|  | 0 | 3 | 2.5705 | 2.9549 | 3.7838 | 1.6190 | 3.5234 | 4.0502 | 5.1865 | 1.1811 |
|  | 1 | 2 | 2.7826 | 3.3629 | 4.6868 | 1.4173 | 3.6908 | 4.4606 | 6.2166 | 1.0685 |
|  | 1 | 3 | 2.6788 | 3.1525 | 4.2538 | 1.5832 | 3.6425 | 4.2866 | 5.7842 | 1.1643 |
| 5 | 0 | 1 | 1.9553 | 2.3655 | 3.4995 | 1.3284 | 2.3647 | 2.8608 | 4.2323 | 1.0984 |
|  | 0 | 2 | 1.9856 | 2.3227 | 3.1370 | 1.6311 | 2.4350 | 2.8483 | 3.8469 | 1.3301 |
|  | 0 | 3 | 2.1419 | 2.4563 | 3.1441 | 1.9484 | 2.7167 | 3.1155 | 3.9880 | 1.5361 |
|  | 0 | 4 | 2.3445 | 2.6525 | 3.2998 | 2.2263 | 3.1115 | 3.5203 | 4.3792 | 1.6776 |
|  | 1 | 2 | 2.3048 | 2.7744 | 2.7744 | 1.7189 | 2.8793 | 3.4658 | 3.4658 | 1.3760 |
|  | 1 | 4 | 2.2953 | 2.6273 | 3.3662 | 2.1368 | 2.9931 | 3.4260 | 4.3896 | 1.6387 |
| 6 | 0 | 1 | 1.7267 | 2.0285 | 2.9784 | 1.5609 | 2.0255 | 2.3795 | 3.4938 | 1.3307 |
|  | 0 | 3 | 1.8642 | 2.1281 | 2.7220 | 2.2506 | 2.2505 | 2.5691 | 3.2860 | 1.8643 |
|  | 0 | 4 | 2.0216 | 2.2833 | 2.8396 | 2.5871 | 2.5207 | 2.8470 | 3.5406 | 2.0749 |
|  | 1 | 2 | 1.9898 | 2.3768 | 3.3072 | 2.0086 | 2.3907 | 2.8557 | 3.9735 | 1.6718 |
| 7 | 0 | 1 | 1.5811 | 1.7966 | 2.5965 | 1.7907 | 1.8149 | 2.0623 | 2.9805 | 1.5600 |
|  | 0 | 2 | 1.5815 | 1.7905 | 2.3987 | 2.1333 | 1.8186 | 2.0590 | 2.7584 | 1.8551 |
|  | 0 | 4 | 1.7990 | 2.0257 | 2.5179 | 2.9176 | 2.1500 | 2.4208 | 3.0091 | 2.4414 |
|  | 0 | 6 | 2.0853 | 2.3132 | 2.7812 | 3.5504 | 2.6553 | 2.9455 | 3.5415 | 2.7883 |
| 8 | 0 | 4 | 1.6374 | 1.8338 | 2.2772 | 3.2261 | 1.8994 | 2.1272 | 2.6416 | 2.7811 |
|  | 1 | 6 | 1.8076 | 2.0123 | 2.4436 | 3.7715 | 2.1665 | 2.4119 | 2.9289 | 3.1466 |
|  | 1 | 7 | 1.9290 | 2.1345 | 2.5571 | 4.0778 | 2.3756 | 2.6287 | 3.1490 | 3.3113 |
| 9 | 0 | 1 | 1.4160 | 1.5300 | 2.0716 | 2.2461 | 1.5794 | 1.7066 | 2.3107 | 2.0137 |
|  | 0 | 3 | 1.4399 | 1.5828 | 2.0022 | 3.0601 | 1.6137 | 1.7738 | 2.2439 | 2.7304 |
|  | 0 | 6 | 1.7125 | 1.8946 | 2.2770 | 4.3367 | 2.0176 | 2.2322 | 2.6827 | 3.6809 |
|  | 1 | 5 | 1.5692 | 1.7481 | 2.1613 | 3.7422 | 1.7951 | 1.9998 | 2.4725 | 3.2713 |
|  | 1 | 6 | 1.6593 | 1.8425 | 2.2364 | 4.1210 | 1.9311 | 2.1442 | 2.6026 | 3.5411 |
|  | 1 | 7 | 1.7607 | 1.9459 | 2.3306 | 4.4741 | 2.0932 | 2.3134 | 2.7708 | 3.7633 |
|  | 1 | 8 | 1.8690 | 2.0552 | 2.4351 | 4.7871 | 2.2775 | 2.5044 | 2.9673 | 3.9285 |
| 10 | 0 | 2 | 1.3429 | 1.4311 | 1.8094 | 2.8306 | 1.4771 | 1.5741 | 1.9902 | 2.5734 |
|  | 0 | 3 | 1.3705 | 1.4805 | 1.8517 | 3.3092 | 1.5155 | 1.6372 | 2.0476 | 2.9926 |
|  | 0 | 5 | 1.5046 | 1.6612 | 2.0219 | 4.2595 | 1.7019 | 1.8790 | 2.2871 | 3.7657 |
|  | 0 | 7 | 1.6786 | 1.8454 | 2.1921 | 5.0739 | 1.9665 | 2.1619 | 2.5680 | 4.3311 |
|  | 1 | 2 | 1.4371 | 1.5849 | 2.1403 | 3.1043 | 1.6026 | 1.7675 | 2.3868 | 2.7837 |
|  | 1 | 3 | 1.4123 | 1.5513 | 2.0463 | 3.2918 | 1.5682 | 1.7226 | 2.2722 | 2.9645 |
|  | 1 | 4 | 1.4206 | 1.5618 | 1.9801 | 3.6330 | 1.5817 | 1.7389 | 2.2047 | 3.2629 |
|  | 1 | 6 | 1.5447 | 1.7078 | 2.0713 | 4.4494 | 1.7586 | 1.9444 | 2.3582 | 3.9081 |
|  | 1 | 8 | 1.7223 | 1.8921 | 2.2414 | 5.2009 | 2.0341 | 2.2346 | 2.6471 | 4.4037 |

Table 5. Parametric values for QSSDSSS-3 ( $n, c^{,} \mathbf{c}_{1}, \mathrm{c}_{2}$ )

| c | $\mathrm{c}_{1}$ | $\mathrm{c}_{2}$ | $\mathbf{n}_{\text {pm }}$ | nAOQL | nAOQL/ $\mathbf{p}_{1}$ | $\mathrm{np}_{1}$ for $\mathbf{0 . 0 5}$ | $\mathrm{h}_{0}$ | np* |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 0 | 1 | 0.9204 | 0.5562 | 0.9394 | 0.5921 | 1.2596 | 1.3207 |
| 3 | 0 | 1 | 0.9365 | 0.7055 | 0.8324 | 0.8475 | 1.8403 | 1.4416 |
|  | 0 | 2 | 1.0813 | 0.8937 | 0.8381 | 1.0663 | 2.5782 | 1.9607 |
| 4 | 0 | 2 | 1.439 | 1.1624 | 0.8548 | 1.3598 | 2.422 | 2.0946 |
|  | 0 | 3 | 1.2633 | 1.0941 | 0.6758 | 1.619 | 3.4061 | 2.7277 |
|  | 1 | 2 | 1.6109 | 1.3802 | 0.9738 | 1.4173 | 3.2276 | 2.3034 |
|  | 1 | 3 | 2.0418 | 1.6998 | 1.0736 | 1.5832 | 2.803 | 2.6412 |
| 5 | 0 | 1 | 1.7484 | 1.4666 | 1.1040 | 1.3284 | 2.6635 | 1.8415 |
|  | 0 | 2 | 1.9876 | 1.6565 | 1.0156 | 1.6311 | 2.7095 | 2.2831 |
|  | 0 | 3 | 1.4591 | 1.2993 | 0.6669 | 1.9484 | 4.2736 | 2.8648 |
|  | 0 | 4 | 1.808 | 1.6025 | 0.7198 | 2.2263 | 4.1408 | 3.5595 |
|  | 1 | 2 | 2.235 | 1.9461 | 1.1322 | 1.7189 | 3.6058 | 2.5135 |
|  | 1 | 4 | 2.7 | 2.2885 | 1.0710 | 2.1368 | 3.0866 | 3.2952 |
| 6 | 0 | 1 | 2.1871 | 1.9035 | 1.2195 | 1.5609 | 3.4652 | 2.0582 |
|  | 0 | 3 | 2.5327 | 2.1699 | 0.9641 | 2.2506 | 3.2237 | 3.0567 |
|  | 0 | 4 | 2.0139 | 1.8244 | 0.7052 | 2.5871 | 5.1154 | 3.696 |
|  | 1 | 2 | 2.4499 | 2.1937 | 1.0922 | 2.0086 | 4.5229 | 2.7505 |
| 7 | 0 | 1 | 3.3932 | 2.9126 | 1.6265 | 1.7907 | 3.3267 | 2.2783 |
|  | 0 | 2 | 3.1548 | 2.7442 | 1.2864 | 2.1333 | 3.5702 | 2.6993 |
|  | 0 | 4 | 1.8673 | 1.3701 | 0.4696 | 2.9176 | 6.0172 | 3.8903 |
|  | 0 | 6 | 2.6723 | 2.1032 | 0.5924 | 3.5504 | 5.5164 | 5.3192 |
| 8 | 0 | 4 | 3.6195 | 2.8703 | 0.8897 | 3.2261 | 4.084 | 4.1064 |
|  | 1 | 6 | 2.8967 | 2.6786 | 0.7102 | 3.7715 | 6.5555 | 5.0485 |
|  | 1 | 7 | 3.6286 | 3.3057 | 0.8107 | 4.0778 | 5.3083 | 5.7385 |
| 9 | 0 | 1 | 4.0737 | 3.664 | 1.6313 | 2.2461 | 4.6266 | 2.7242 |
|  | 0 | 3 | 4.5384 | 4.0144 | 1.3119 | 3.0601 | 4.0215 | 3.7034 |
|  | 0 | 6 | 2.6417 | 2.4769 | 0.5711 | 4.3367 | 8.1229 | 5.6407 |
|  | 1 | 5 | 4.117 | 3.7838 | 1.0111 | 3.7422 | 5.9112 | 4.6591 |
|  | 1 | 6 | 3.4512 | 3.2077 | 0.7784 | 4.121 | 6.9175 | 5.2614 |
|  | 1 | 7 | 3.8757 | 3.5792 | 0.8000 | 4.4741 | 6.2956 | 5.9132 |
|  | 1 | 8 | 4.3297 | 3.9604 | 0.8273 | 4.7871 | 5.5317 | 6.6303 |
| 10 | 0 | 2 | 4.796 | 4.333 | 1.5308 | 2.8306 | 4.8118 | 3.3369 |
|  | 0 | 3 | 2.4991 | 2.3514 | 0.7106 | 3.3092 | 8.5085 | 3.922 |
|  | 0 | 5 | 2.8502 | 2.6901 | 0.6316 | 4.2595 | 9.1031 | 5.2057 |
|  | 0 | 7 | 3.8597 | 3.6136 | 0.7122 | 5.0739 | 7.8445 | 6.5366 |
|  | 1 | 2 | 5.8482 | 5.26 | 1.6944 | 3.1043 | 4.6471 | 3.7568 |
|  | 1 | 3 | 6.3418 | 5.6112 | 1.7046 | 3.2918 | 4.1265 | 3.9413 |
|  | 1 | 4 | 3.1597 | 2.9554 | 0.8135 | 3.633 | 7.5421 | 4.3507 |
|  | 1 | 6 | 3.3373 | 3.1315 | 0.7038 | 4.4494 | 7.9697 | 5.4908 |
|  | 1 | 8 | 4.1231 | 3.8468 | 0.7396 | 5.2009 | 7.3284 | 6.8025 |

### 5.2. Construction of Table 3, Table 4 and Table 5

Under the assumption of poisson model, the OC function of QSSDSS -3 $\left(\mathrm{n} ; \mathrm{c} ; \mathrm{c}_{1}, \mathrm{c}_{2}\right)$ is given by

$$
\begin{equation*}
P a(p)=\frac{P_{N} P_{T}^{3}+P_{T}\left(1-P_{N}\right)\left(P_{T}^{2}+P_{T}+1\right)}{P_{T}^{3}+\left(1-P_{N}\right)\left(P_{T}^{2}+P_{T}+1\right)} \tag{1}
\end{equation*}
$$

Under the assumption of the poisson model $\mathrm{Pa}(\mathrm{p})$ is solved for using the equation (1) in MATLAB program and we get the different np values. The values are presented in Table 3. Using Table 3, for assumed values of $\alpha$ and $\beta$, the operating ratio $\mathrm{p}_{2} / \mathrm{p}_{1}$ is calculated and the values are presented in Table 4. Using the $\mathrm{np}_{0}$ values given in Table 3, the relative slope $\mathrm{h}_{0}$ is evaluated and these values are provided in Table 5 for specified values of QSSDSS - 3 ( $n, c_{1}, c_{1}, c_{2}$ ).

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